# Properties and characterization of low-temperature amorphous PECVD silicon nitride films for solar cell passivation

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Deposition conditions and some structural and electrical properties of amorphous silicon nitride (Si<sub>x</sub>N<sub>y</sub>:H) films deposited on Si substrates have been studied for photovoltaic applications. A plasma enhanced chemical vapor deposition (PECVD) system has been used for the study. Experiments have been performed varying the flow ratios and dilution of the reactant gases. Increased hydrogen (H<sub>2</sub>) dilution leads to reduced deposition rate and a better controllability in the growth process. The hydrogen content in the film also decreases with increasing H<sub>2</sub> dilution of the reactant gases. Flow ratio of the reactant gases (SiH<sub>4</sub>/NH<sub>3</sub>) also influences the growth rate. There is an optimal reactant gas mix to maximize the film growth rate. However, the film stoichiometry is also modified by changing the gas mix, with higher flow ratios resulting in Si-rich films. The level of interfacial recombination of minority carriers has been studied by capacitance-voltage and effective lifetime measurements. Bombardment by the energetic species in the plasma leads to plasma damage at the interface. These interfacial defects can be annealed by a post-deposition, low temperature treatment. © *2005 Springer Science + Business Media, Inc.* 

### 1. Introduction

Amorphous silicon nitride  $(Si_xN_y:H)$  deposited by plasma enhanced chemical vapor deposition (PECVD) has been a topic of intensive investigation in the past several years. Studied plasma deposition techniques include electron cyclotron resonance (ECR) plasma [1], remote [2] and RF [3] plasma, to name a few. Plasma nitrides have a wide range of applications such as gate dielectrics in thin film transistors, metal-insulatorsemiconductor field effect transistors [4–6], as well as encapsulation layers for electronic devices. Moreover,  $Si_x N_y$ :H films have also been found to be very useful in crystalline Si photovoltaic (PV) devices [see for example, 7–9]. In Si PV cells, the nitride films provide an efficient passivation by reducing the surface recombination velocity at the Si/Si $_x$ N $_y$  interface. It is also possible to achieve hydrogen passivation of Si bulk defects by the nitride process. This is especially important when low cost Si materials such as multicrystalline Si, Si ribbons etc., are used as substrates. In addition to these advantages,  $Si_x N_y$ : H films also act as anti-reflection coatings on the solar cell surface. The structure and stoichiometry of low temperature deposited amorphous  $Si_xN_y$ :H films are complicated and are strongly influenced by deposition conditions such as, the type of plasma excitation, temperature, pressure, gases and flow rates. In addition, any plasma-induced damage at the Si/Si<sub>x</sub> $N_{y}$  interface is also very critical in the surface passivation of Si PV cells. Techniques such as hot wire CVD [10] and remote plasma CVD [7] result in minimal or no surface damage. In this work we perform various sets of experiments in a PECVD nitride deposition system in order to gain a comprehensive understanding of the effect of processing conditions on the film and interfacial properties. Structural and electrical properties of the nitride films as well as the influence of postdeposition thermal treatments on any eventual plasmainduced damage at the interface are investigated.

### 2. Experimental

## 2.1. Film deposition and sample preparation

The hydrogenated  $Si_xN_y$ :H films were deposited on *p*-type Si wafers in a conventional parallel plate 13.56 MHz PECVD deposition system. The wafers were always cleaned using the standard RCA solutions and HF-dipped prior to being loaded in the system. We used SiH<sub>4</sub> and NH<sub>3</sub> as precursor gases and H<sub>2</sub> as a dilutant. The ratio between SiH<sub>4</sub> and NH<sub>3</sub> gas flows, as well as the degree of H<sub>2</sub> dilution was varied for various experiments. The depositions were carried out at 300°C with the RF power kept at 25 W. Table I summarizes the experimental matrix. For the Fourier Transform

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TABLE I Flow ratios of the reactant gases and the degree of hydrogen dilution used for the deposition of the  $Si_xN_y$ :H films

Sample #	Flow ratio of SiH <sub>4</sub> /NH <sub>3</sub> (sccm/sccm)	Hydrogen dilution (sccm)
N1	5/50	0
N2	5/50	30
N3	5/50	60
N4	5/50	90
N5	10/50	0
N6	10/50	30
N7	10/50	60
N8	10/50	90
N9	10/20	0
N10	10/20	30
N11	10/20	60
N12	10/20	90

Infrared Spectroscopy (FTIR) analysis, the Si wafers were deposited with relatively thicker (1  $\mu$ m) nitride films. For the analysis of interface trap density ( $D_{it}$ ) Al/Si<sub>x</sub>N<sub>y</sub>:H/Si/Al capacitors were fabricated by sputtering Al on nitride-coated Si samples followed by patterning into arrays of capacitor structures (36756  $\mu$ m<sup>2</sup>) using photolithography. The nitride film thickness in each case was measured by a surface profilometer on patterned steps on the film. For the effective minority carrier lifetime ( $\tau_{eff}$ ) measurements by RF Photoconductivity Decay (RF-PCD) method, Si samples were coated with nitride on both sides under identical conditions. The lifetime samples underwent post-deposition anneals in a clean furnace at various temperatures in the range of 350–475°C in N<sub>2</sub> ambient.

#### 2.2. FTIR measurements

FTIR measurements were carried out in the 400 to  $4000 \text{ cm}^{-1}$  range, for the Si<sub>x</sub>N<sub>y</sub>:H films deposited with different SiH<sub>4</sub>/NH<sub>3</sub> ratios and H<sub>2</sub> dilutions. A baseline correction was performed. Peaks corresponding to Si–H and N–H bonds were identified from the absorption spectra and the relative densities of the bonds were determined, from which the H-content was calculated using standard technique.

#### 2.3. Capacitance-voltage (C-V) measurements

High frequency (1 MHz) C-V characteristics of the fabricated Al/Si<sub>x</sub>N<sub>y</sub>:H/Si/Al capacitor structures were measured using a Keithley Model 590 CV system. The sample was kept in the dark and 5 measurements were taken in different places for each sample. The C-V curves were then used to calculate the interface trap density ( $D_{it}$ ) at the Si<sub>x</sub>N<sub>y</sub>:H/Si interface.

#### 2.4. Effective minority carrier lifetime measurements

Radio-frequency Photoconductivity Decay (RF-PCD) measurements were performed to determine the effective minority carrier lifetime ( $\tau_{eff}$ ) of the sample coated on both sides with Si<sub>x</sub>N<sub>y</sub>:H films. The measurement

system uses a 532 nm laser pulse for excitation. The decay of the photoconductivity with time is recorded, from which  $\tau_{eff}$  is extracted from the slope of the linear portion of the decay profile [11]. For each wafer, 5 measurements were taken at different places and the values were averaged.

#### 2.5. Post-deposition thermal annealing

The lifetime samples were annealed in a clean, opentube, quartz furnace in N<sub>2</sub> ambient at different temperatures in the range of 350–475°C. The effective lifetime was measured again on these samples in order to investigate the annealing of plasma-induced defects at the Si<sub>x</sub>N<sub>y</sub>:H/Si interface.

## 3. Results and discussion

#### 3.1. Film deposition rate

Fig. 1 shows the deposition rate of  $Si_x N_y$ :H films as a function of H<sub>2</sub> dilution in the plasma chamber for various SiH<sub>4</sub>/NH<sub>3</sub> gas ratios. Within the set of parameters used in our experiments, the general trend that we observe is that the growth rate decreases with increasing hydrogen dilution, irrespective of the SiH<sub>4</sub>/NH<sub>3</sub> ratio. With increasing hydrogen dilution the partial pressures of the reactive gases are reduced. Therefore the availability of the reactants is diminished, leading to a reduction in deposition rate. The reduction in partial pressure can also help eliminate/reduce gas phase reactions which usually produce larger molecules that lead to poor quality films. With increased hydrogen dilution, the plasma-generated hydrogen atoms can cause saturation of hydrogen-lacking radicals, especially those of NH<sub>3</sub>. This will also reduce the deposition rate. The data in Fig. 1 shows that one can achieve a good control on growth rate by hydrogen dilution even when other parameters such as RF power and temperature are kept constant. Another important observation from Fig. 1 is that the dependence of the deposition rate on the SiH<sub>4</sub>/NH<sub>3</sub> flow ratio. The data consistently show that, for any given H<sub>2</sub> dilution, the deposition rate passes through a "maximum": the deposition



*Figure 1* Deposition rate of Si<sub>x</sub>N<sub>y</sub>:H films as a function of hydrogen dilution of reactant gases for various flow ratios of the reactant gases.

rates corresponding to a flow ratio of 0.2 (= 10/50) is always higher than those corresponding to flow ratios of 0.5 (=10/20) and 0.1 (=5/50). This suggests there is a balanced gas phase Si and N density that will lead to the highest deposition rate. On the other hand, it is important to note that varying the SiH<sub>4</sub>/NH<sub>3</sub> flow ratio will vary the stoichiometry of the deposited film resulting in very different electrical and structural properties.

#### 3.2. Film composition

Fig. 2 shows the absorption bands corresponding to Si–H stretching vibrations (2160 cm<sup>-1</sup>) for Si<sub>x</sub>N<sub>y</sub>:H films deposited with 3 different SiH<sub>4</sub>/NH<sub>3</sub> flow ratio and with zero H<sub>2</sub> dilution. Among the 3 flow ratios that we have used, the highest flow ratio (0.5) results in the largest Si–H peak. Similarly Fig. 3 shows the absorption bands due to N–H stretching vibrations



*Figure 2* FTIR spectra of the absorption bands corresponding to Si-H stretching vibrations in the nitride films deposited using different gas flow ratios (without  $H_2$  dilution).



*Figure 3* FTIR spectra of absorption bands corresponding to N-H stretching vibrations in the nitride films deposited using different gas flow ratios (without  $H_2$  dilution).



*Figure 4* Intensity of Si–H bonds as extracted from the FTIR spectra for all the samples different  $H_2$  dilutions and reactant gas flow ratios.



*Figure 5* Intensity of N–H bonds as extracted from the FTIR spectra for all the samples different  $H_2$  dilutions and reactant gas flow ratios.

(3350 cm<sup>-1</sup>), for zero H<sub>2</sub> dilution, where the trend is just the opposite: the highest flow ratio (0.5) results in smallest N-H peak. This is somewhat expected: as the SiH<sub>4</sub>/NH<sub>3</sub> flow ratio is increased (0.1 to 0.5) the films are expected to have a high Si content. The same trend was observed for other levels of H<sub>2</sub> dilution as well. Figs. 4 and 5 show the complete data (all flow ratios and H<sub>2</sub> dilutions) for the Si-H and N-H absorbance peaks respectively. With increasing H<sub>2</sub> dilution the dependence of N-H and Si-H intensities on the flow ratio seems to be slightly decreasing. Further, with increasing H<sub>2</sub> dilution, the strongest peaks (i.e., Si-H for a flow ratio of 0.5, and N–H for a flow ratio of 0.1) drop more significantly compared to the peaks of other flow ratios. Fig. 6 shows the H-content in the films for all the cases considered. The H-content has been deduced from the FTIR spectra [12]. The general trend is that the H content in the film decreases with increasing  $H_2$ dilution. This can be attributed to the mechanism in which H atoms saturate the species lacking single hydrogen. Such species, when adsorbed to the surface, can add to the H-content in the film. By removal of those species, radicals with fewer H atoms take part more in the surface reactions, resulting in films with lower H-content. A closer look at Fig. 6 reveals that the decrease of H-content in Si-rich samples (mainly stemming from Si-H bonds) is not as steep as that in N-rich samples (mainly stemming from N-H bonds) as H<sub>2</sub> dilution is increased. This implies that hydrogen interacts with species originating from NH3 more substantially than SiH<sub>4</sub> radicals.

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Figure 6 Hydrogen content in the nitride films deposited with different  $H_2$  dilution of the reactant gases and reactant gas flow ratios.

#### 3.3. C-V measurements: Interface trap density

The density of the interface traps  $(D_{it})$  has been estimated from the measured high frequency C-V curves using the Terman method [13]. In this method the measured data is compared to an ideal theoretical curve and the  $D_{it}$  is extracted as a function of position in the Si bandgap. Fig. 7 shows a typical  $D_{it}$  curve obtained for the  $Si_x N_y$ :H/Si interface where the film was deposited with a SiH<sub>4</sub>/NH<sub>3</sub> flow ratio of 0.1 (5/50) and without  $H_2$  dilution. The  $D_{it}$  at the midgap (0.56 eV) is found to be around  $9.93 \times 10^{11}$  cm<sup>-2</sup> eV<sup>-1</sup>. These values indicate that the interface quality can still be improved. Table II gives the mid-gap  $D_{it}$  values obtained on several of our capacitors. The values are in the  $10^{11}$ – $10^{12}$ range, and are rather scattered. Since we use a PECVD system for the film deposition, the interface has been exposed to bombardment by energetic species. Therefore there is a high possibility that there has been significant plasma-induced damage at the interface, and that this negative effect has been dominant in all the samples. Note that the RF power (25 W), pressure (150 mTorr) and deposition time (25 min) were kept constant for all our capacitor samples. We have verified the interface



*Figure 7* A typical interface trap density profile as extracted from high frequency C-V measurements on one of the Si<sub>x</sub>N<sub>y</sub>:H/Si capacitors. (ni-tride deposition condition: SiH<sub>4</sub>/NH<sub>3</sub> = 5/50, without H<sub>2</sub> dilution).

TABLE II Interface trap density  $(D_{it})$  of different samples extracted from high frequency capacitance-voltage (C-V) measurements

SiH <sub>4</sub> /NH <sub>3</sub> flow rate (sccm/sccm)	H <sub>2</sub> dilution (sccm)	Interface trap density at midgap ( $cm^{-2} eV^{-1}$ )	
5/50	0	$9.93 \times 10^{11}$	
5/50	30	$9.19 \times 10^{11}$	
5/50	60	$2.71 \times 10^{12}$	
5/50	90	$3.5 \times 10^{12}$	
10/50	0	$9.56 \times 10^{11}$	
10/50	30	$3.08 \times 10^{12}$	
10/50	60	$1.46 \times 10^{12}$	
10/50	90	$2.80 \times 10^{12}$	

damage effect by subjecting some of the samples to post-deposition defect anneals. This is explained in the next section.

#### 3.4. Effective minority carrier lifetime and post-deposition defect anneal

The effective lifetime  $(\tau_{eff})$  of the minority carriers was measured on wafers coated on both sides with  $Si_x N_y$ :H films. Fig. 8 shows the photoconductivity decay curve for the sample with films on both sides deposited with a 5/50 gas flow ratio and 30 sccm H<sub>2</sub> dilution. The  $\tau_{\rm eff}$ value extracted from the decay curve contains both the bulk and surface recombination components with the relationship,  $1/\tau_{eff} = 1/\tau_b + 2S/d$ , where " $\tau_b$ " is the bulk lifetime, "S" the surface recombination velocity, and "d" is the sample thickness. Therefore any changes in  $\tau_{\rm eff}$  after processes carried out at low temperatures can indicate a change in the surface passivation level provided the bulk lifetime is not affected. The values of  $\tau_{\rm eff}$  obtained for our samples were quite scattered irrespective of the film deposition conditions. This, as has been discussed in the previous section, again indicates the possibility of plasma damage causing interfacial recombination. To further investigate this, we



*Figure 8* A typical photoconductivity decay profile of a nitride-coated Si sample. (nitride deposition condition:  $SiH_4/NH_3 = 5/50$ ,  $H_2$  dilution = 30 sccm).

TABLE III Measured effective lifetime ( $\tau_{eff}$ ) of nitride coated Si samples after being subjected to different temperature treatments. (conditions used for nitride deposition: SiH<sub>4</sub>/NH<sub>3</sub> flow ratio = 5/50, H<sub>2</sub> dilution = 30 sccm)

Post-deposition annealing condition	Effective lifetime, $\tau_{\rm eff}$ (µs)	
as-deposited (no anneal)	14.45	
350°C, 30 min	26.53	
400°C, 30 min	21.55	
425°C, 30 min	14.07	
475°C, 30 min	10.63	

TABLE IV Effective lifetime ( $\tau_{eff}$ ) of as-deposited and annealed samples. (annealing condition has been 350°C, 30 min for all samples)

SiH <sub>4</sub> /NH <sub>3</sub> flow ratio (sccm/sccm)	H <sub>2</sub> dilution (sccm)	Efective lifetime: as-deposited (µs)	Effective lifetime: after $350^{\circ}$ C/30 min anneal ( $\mu$ s)
5/50	0	16.53	45.2
5/50	30	14.45	26.53
5/50	60	8.74	13.9
5/50	90	13.07	19.52
10/50	0	14.23	23.56
10/50	30	8.19	27.59
10/50	60	11.57	25.97
10/50	90	13.23	26.51
10/20	0	9.07	32.08
10/20	30	8.69	20.73
10/20	60	7.47	10.73
10/20	90	11.3	17.99

have subjected pieces of the sample to different thermal annealing treatments and measured the lifetime again. For example, the  $\tau_{eff}$  corresponding to the decay in Fig. 8 is 14.45  $\mu$ s. Table III shows the  $\tau_{eff}$  of different pieces of the same sample after being subjected to different thermal anneals. Lower temperatures (<400°C) cause an improvement in  $\tau_{\rm eff}$ , indicating defect annealing. Higher temperatures however, seem to be causing the lifetime to drop again, most probably due to hydrogen loss from the interface leading to a poor passivation. This is quite possible because the annealing time was long (30 min). Table IV gives the  $\tau_{eff}$  values of as-deposited and thermally annealed (350°C, 30 min) samples for different film deposition conditions. The lifetime improvement after the 350°C anneal is consistent in all the samples. In Table IV, the  $\tau_{\rm eff}$  of one sample cannot be compared to that of another sample because the bulk lifetime  $(\tau_b)$  may be different. However, the improvement in surface passivation after the defect anneal is evident in all samples.

#### 4. Conclusions

We have used a plasma PECVD system to study the properties of amorphous Si<sub>x</sub>N<sub>y</sub>:H films. Several experiments have been performed varying the flow ratios of the reactant gases and hydrogen dilution. Increased hydrogen dilution leads to reduced deposition rate and a better controllability in the growth process. The hydrogen content in the film also reduces with increasing  $H_2$ dilution of the reactant gases. Flow ratio of the reactant gases (SiH<sub>4</sub>/NH<sub>3</sub>) also changes the growth rate. There seems to be an optimal reactant gas mix to maximize the growth rate. However, the film stoichiometry is modified by changing the flow ratio. Higher flow ratios result in Si-rich films. The level of interfacial recombination of minority carriers has been studied by  $D_{it}$ analysis through C-V measurements, and by effective lifetime measurements. Bombardment by the energetic species in the plasma leads to plasma damage at the interface. The interfacial defects can be annealed by a post-deposition, low temperature treatment.

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